



Conference Paper

Statistical Approach to Estimated Uncertainty of Nuclear Concentration in Problems of Isotope Kinetics

V. V. Kolesov, A. V. Novichkov, E. E. Voznyakevich, and A. M. Terekhova

Obninsk Institute for Nuclear Power Engineering of the National Research Nuclear University MEPhI, Studgorodok 1, Obninsk, Kaluga region, 249040, Russia

Abstract

The minority of papers only is devoted to the study of impact of the uncertainties in nuclear data on the nuclear concentration received during the solution of the problem of fuel burn-up in the reactor facility. On the other hand, uncertainties of known reaction rates, neutron fluxes, etc. can lead to considerable distortions of the results obtained therefore it is important to be able to assess the impact of such uncertainties on nuclear concentration of nuclides. In this paper we consider the problem of the impact assessment of uncertainties in nuclear data on reactor functionalities as applied to isotope kinetics which represents the well-known Cauchy linear problem. The most exact approach is the statistical approach of the randomized selection of input parameters in using different distribution laws. But the simplest method of the analysis of sensitivity of model to perturbation parameters is the following (it has several names in the literature: one-at-a-time sensitivity measures, 1% sensitivity method): by varying one of the input parameters of the task for the small amount (for example, for 1%) when other parameters are constant, the corresponding response of output parameters is defined (variation approach). Our results show that in burn-up calculations the mean square deviations of nuclear concentrations obtained using statistical approach coincide with the variations of nuclear concentrations obtained in the variation approach.

Keywords: reactor facility, burn-up calculations, statistical approach, variation approach, nuclear data uncertainties, nuclear concentration uncertainties.

1. Introduction

At the present day much attention is given to the assessments of the impact of uncertainties in nuclear data on parameters of various reactor facilities. However, in general the impact of uncertainties in nuclear data on standard functionalities (K_{eff} , reaction rates etc.) obtained using sensitivity coefficients. The minority of papers only is

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Corresponding Author:

VVKolesov@mephi.ru

V. V. Kolesov

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devoted to the study of impact of the uncertainties in nuclear data on the nuclear concentration received during the solution of the problem of fuel burn-up in the reactor facility ([1–3]). The solution of fuel burn-up problems is important for assessment of accumulation of a number of isotopes arising in reactor facilities, such as, for example, of plutonium isotopes. At the same time in general it is rather difficult to determine experimentally their concentration in the spent fuel. Thus, numerical methods of solution of burn-out problems are of high importance now. On the other hand, uncertainties of known reaction rates, neutron fluxes, etc. can lead to considerable distortions of the results obtained therefore it is important to be able to assess the impact of such uncertainties on nuclear concentration of nuclides.

Propagation of uncertainties in nuclear data on the parameters which characterize the nuclear facility can be executed in a number of ways. At the present day the most known approach is an approach for obtaining the sensibility coefficients defined by the linear perturbation theory. In the end we obtain the linear equation system with respect to sensitivity coefficients.

The simplest method of the analysis of sensitivity of model to perturbation parameters is the following (it has several names in the literature: one-at-a-time sensitivity measures, 1% sensitivity method): by varying one of the input parameters of the task for the small amount (for example, for 1%) when other parameters are constant, the corresponding response of output parameters (see e.g. [4]) is defined.

However, the most exact approach is the statistical approach of the randomized selection of parameters using different distribution laws. At the same time we can run both one and several parameters of the model considering them as independent parameters or with use of correlation between them.

Let us consider the problem of the impact assessment of uncertainties in nuclear data on reactor functionalities as applied to isotope kinetics which represents the well-known Cauchy linear problem.

As per [5] let the differential equation system of the first order (in case of isotope kinetics – linear) be given for definition of nuclear concentration vector $\vec{N}(t, \vec{p})$ of *n* dimension:

$$\frac{d\vec{N}(t,\vec{p})}{dt} = f(t,\vec{N}(t,\vec{p}),\vec{p}) = K(\vec{p})\vec{N}(t,\vec{p})$$
$$\vec{N}(0,\vec{p}) = \vec{N}_0(\vec{p}),$$

where $K(\vec{p})$ - matrix of coefficients which depend on problem parameters (vector of parameters $\vec{p} = (p_1, ..., p_m)$), such as one-group neutron flux density, one-group reaction rates for different nuclides, etc.



Perturbed solution $\vec{N}(t, \vec{p}) + \Delta \vec{N}(t, \vec{p})$, which corresponds to the perturbed parameter column $\vec{p}_i + \Delta \vec{p}_i$ can be determined in the predicate of linear expansion (linear perturbation theory):

$$N_i(t, \vec{p} + \Delta \vec{p}) \approx N_i(t, \vec{p}) + \frac{\partial N_i(t, \vec{p})}{\partial p_i} \Delta p_i$$

Whereby it is necessary to solve the problem with regards to the perturbations:

$$\frac{d\Delta \vec{N}(t,\vec{p})}{dt} = \frac{\partial \vec{f}(t,\vec{p})}{\partial \vec{N}} \Delta \vec{N}(t,\vec{p}) + \frac{\partial \vec{f}(t,\vec{p})}{\partial \vec{p}} \Delta \vec{p};$$
$$\Delta \vec{N}(0,\vec{p}) = 0,$$

Where elements of the matrix $\frac{\partial \vec{f}(t,\vec{p})}{\partial \vec{N}} \equiv \begin{bmatrix} \frac{\partial f_i(t,\vec{p})}{\partial N_k} \end{bmatrix}$ of size: $n \times n$ and elements of the matrix $\frac{\partial \vec{f}(t,\vec{p})}{\partial \vec{p}} \equiv \begin{bmatrix} \frac{\partial f_i(t,\vec{p})}{\partial p_k} \end{bmatrix}$ of size: $n \times m$, broadly speaking, depend on t and, therefore they should be calculated on every step which involves a certain difficulty.

The so-called sensibility factors are often introduced; the matrix hereof is given by: $Z(t, \vec{p}) \equiv \frac{\partial \vec{N}(t, \vec{p})}{\partial \vec{p}} \equiv \left[\frac{\partial N_i(t, \vec{p})}{\partial p_k}\right] \text{ and it depends on } t.$

These factors can be estimated from the system $m \times n$ of linear equations:

$$\frac{dZ_{ik}(t,\vec{p})}{dt} = \frac{\partial f_i(t,\vec{p})}{\partial \vec{N}_k} Z_{ik}(t,\vec{p}) + \frac{\partial f_i(t,\vec{p})}{\partial \vec{p}_k};$$
$$Z_{ik}(0,\vec{p}) = 0.$$

Application of the linear perturbation theory for problems of isotope kinetics are considered, for example, in [1] and [2].

In statistical approach let us consider that any of p_i parameters is known with some uncertainty. Then p_i is a random variable distributed under the lognormal law with the given mean value and variance (mean square deviation).

Let us study the impact of uncertainties in nuclear data on nuclear concentration of the nuclides obtained during solution of the problem of fuel burn-up, running the corresponding random variable with the given mean square deviation.

VisualBurnOut [6] was used as the program for calculation of fuel burn-up where, in turn, the one-group reaction rates and fluxes assumed in the special format which corresponded to the output format of the MCNP [7] program were used.

2. Calculation results

In order to study the impact of uncertainties of reaction rates on nuclear concentration let us consider the problem of fuel burn-up in the benchmark cell which represents a



three-zone square cell (lattice spacing is 1.3127 cm) with MOX fuel [8]. The structure of physical zones is given in Table 1.

N×10 ²⁴ 1/cm ³	Fuel ($PuO_2 + UO_2$), T = 900K	Clad (zircaloy), T=620K, outer diameter - 0.475 cm, thickness - 0.065 cm	Moderator (H ₂ O), T=575K
²³⁴ U	0.0000027043		
²³⁵ U	0.00005657		
²³⁸ U	0.022286		
²³⁸ Pu	0.0000045941		
²³⁹ Pu	0.0008564		
²⁴⁰ Pu	0.000054669		
²⁴¹ Pu	0.0000027221		
²⁴² Pu	0.000004518		
0	0.046515		
Zr (nat)		0.038657	
Fe(nat)		0.00013345	
Cr(nat)		0.000068254	
¹ H			0.048414
¹⁶ 0			0.024213
¹⁰ B			0.0000047896
¹¹ B			0.000019424

TABLE 1: The structure of the cell used for burn-up calculations.

During execution of calculations of burn-up we assumed that mean square deviations of rates of fission and radiative capture of ²³⁵U and ²³⁹Pu made 10%. According to the lognormal distribution law the corresponding reaction rate was repeatedly run, and every time the burn-up problem was solved. Burn-up calculations at perturbation of rates of fission and radiative capture were respectively performed for effective burnup periods of 100 and 500 days. The reaction rates were run 3000 times for obtaining the mean square deviations of nuclear concentration. In the course of calculations the neutron flux density assumed to be a constant.

As a result we obtained the random selection of nuclear concentration of nuclides. For example Figures 1 and 2 present the diagrams of distribution of nuclear concentrations 90 Y (for 100 days) and 238 Pu (for 500 days).





Figure 1: Distribution of nuclear concentration 90 Y at 10% perturbation of 235 U and 239 Pu fission rate at burn-up within 100 days and neutron flux density F = $3 \cdot 10^{14}$ cm⁻²s⁻¹.



Figure 2: Distribution of nuclear concentration 238 Pu at 10% perturbation of 235 U and 239 Pu radiative capture rate at burn-up within 100 days and neutron flux density F = $3 \cdot 10^{14}$ cm⁻²s⁻¹.

The results obtained by us for mean square deviations of nuclear concentration were compared to the results obtained by means of the so-called one-at-a-time sensitivity measures (hereinafter referred to as variation approach). The main point of these approaches as already mentioned is the variation of any input parameter and study of the impact of this variation for the output parameters. In this approach the variation of the rates made also 10% and we studied the obtained variations in nuclear concentrations.



If several reaction rates varied, the calculation of the full variation was performed as follows:

$$total$$
var = $\sqrt{\sum_{i=1}^{n} var_{i}^{2}}$

The result obtained by us for both approaches are given in tables 2 and 3.

TABLE 2: Comparison of statistical and variation approach for assessment of uncertainties of nuclear concentration of $^{90}{\rm Y}.$

Statistical approach (n of the run reaction period –	nean square deviations rate – 10%, burn-out 100 days)	Variation approach (variation of reaction rate- 10%, burn-out period – 100 days)		
Run parameter	Nuclear concentration of ⁹⁰ Y and its mean square deviation (in %)	Run parameter	Nuclear concentration of ⁹⁰ Y and its variation (in %)	
²³⁵ U fission rate	4.92·10 ¹⁴ +/-0.82	²³⁵ U fission rate	4.92·10 ¹⁴ +/-0.81	
²³⁹ Pu fission rate	4.92·10 ¹⁴ +/-7.62	²³⁹ Pu fission rate	4.92·10 ¹⁴ +/-7.63	
Total fission rates of ²³⁵ U and ²³⁹ Pu	4.92·10 ¹⁴ +/-7.66	Total fission rates of ²³⁵ U and ²³⁹ Pu	4.92·10 ¹⁴ +/-7.67	

TABLE 3: Comparison of statistical and variation approach for assessment of uncertainties of nuclear concentration of ²³⁸Pu.

Statistical approach (mean square deviations of the run reaction rate – 10%, burn-out period – 500 days)		Variation approach (variation of reaction rate- 10%, burn-out period – 500 days)		
	Run parameter	Nuclear concentration of ²³⁸ Pu and its mean square deviation (in %)	Run parameter	Nuclear concentration of ²³⁸ Pu and its variation (in %)
	²³⁵ U fission rate	7.38·10 ¹⁷ +/-0.26	²³⁵ U fission rate	7.38·10 ¹⁷ +/-0.26
	²³⁹ Pu fission rate	7.38·10 ¹⁷ +/-0.89	²³⁹ Pu fission rate	7.38·10 ¹⁷ +/-0.87
	Total fission rates of ²³⁵ U and ²³⁹ Pu	7.38·10 ¹⁷ +/-0.93	Total fission rates of ²³⁵ U and ²³⁹ Pu	7.38·10 ¹⁷ +/-0.91

3. Conclusions

The results of the conducted studies show that the mean square deviations of nuclear concentration obtained using statistical approach coincide with the variations of nuclear concentrations obtained in the variation approach. Thus, for assessment of impact of uncertainties of reaction rates on the nuclear concentration obtained from



the solution of the problem of burn-up it is possible to use less labor-consuming variation approach for assessment of their uncertainties.

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